

March 9-1904

On Miller's West line measured  
from Big-burn oak set  
stake at 5 ch. said by deed  
to be dist to sec <  
fence and line at 54'

On S. line Sec. 4 - T. 3. R. 13 -  
from Stone SW<sup>1</sup> Sec - large stone  
dug out from under 6" of dirt  
+ on top 4" -

At 5.50 center Lewis creek.

" 10+11 lks. line south.

" 20.22

" 29.11 cor. just < Miller which  
is 54' from oak (see opp. page)

At 40. set stake

" 40.40 center road

" 34.75 Lewis Creek.

" 45.65

" 57.60 old mill race

" 66.23 chin Mohr - Dan Hurst -  
on south north

" 72.75 Lewis Creek

" 80.48 1/2 sec < stone.

Found this stone in frame under  
6" soil

On South line Sec 34-T. 4, R. 13.  
Measured East from Stone  
S6 Sec. 4 & SW2 Sec 34

- At 19.70 Shawandook Creek  
" 40.53 fence line Ed Hunt &  
Ero. Stuts north and Sam Hunt  
↑ Faulkner south -  
" 45.10 Graves creek  
" 54.17 line on South-Faulkner  
& Mary S. Adams  
" 60.61 oak stump, supposed to  
be witness tree -  
" 69. Graves creek  
" 73 " "  
" set stake at 80.  
" center pipe from north  
80.94

Measured from stone SW<sup>1</sup>/<sub>4</sub> Sec 3 -  
north at 40.52 point claimed  
for  $\frac{1}{4}$  <  
Set stake at 80.00 and dug  
for < at 81.04



70  
+255  
66  
65

9.999965: 9.999997 =  
1.908539 = 81.01  
1.908536  
9.999965  
1.908568 = 81.02

State.

60  
+995  
58  
55



120-13  
55-52 1/2  
176-05 1/2  
3-58 1/2

State.

9.826597: 9.936598  
0.915501  
10.742079  
8.875299  
1.908792 =  
80.50  
.09  
80.61

50

20.02  
924.00

3-58 1/2

8.874456: 9.936598  
0.915501  
10.742079  
8.875299  
1.908792 =  
80.84

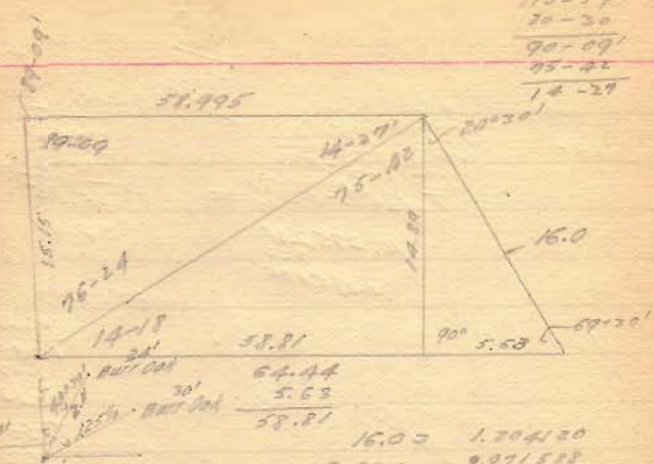
45

8.830607  
9.5  
1.877572: 9.986597  
0.915501  
10.742079  
8.875299  
1.908792 = 81.01  
80.84

40

1.908792 = 81.01  
80.84

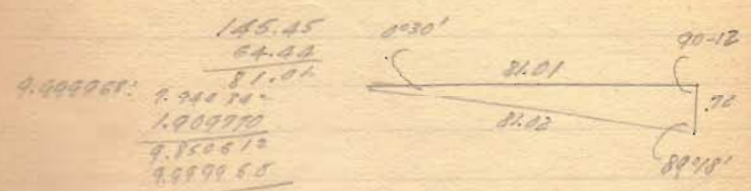
110-39  
70-30  
90-09  
75-22  
14-29



Set 8' to 5' at this point.

1.204120  
7.544725 = 20-30  
10.745445 = 5.63  
1.759451 = 51.81  
7.926231 = 78.42  
1.978124 = 60.69  
1.204120  
1.175708 = 10.19  
7.569451 = 58.81  
9.406257 = 14-18  
16.00  
5.63  
1.704120  
7.569451 = 9.971588  
1.175708 = 14.29

9.999952: 9.997122  
1.983120 = 60.09  
11.180252  
9.999952  
145.45  
64.44  
1.190000 = 15.15  
14.43  
0.72  
89-09  
14-27  
103-36  
88-24  
14-18  
90-42



9.999965: 9.940744  
1.909770  
9.850612  
9.899965  
8.850644

64.44  
.09  
64.53  
81.02  
.09  
81.02  
State 80.84



1/4 Cor. S side Sec. 21-5-13

$T. 62-03 \frac{3}{4} = 10.275470$

$\frac{55.47 \frac{1}{2}}{117-51}$   
 $6-16 \frac{1}{2}$

+ 25.5

176

$\frac{40.45}{5.00}$   
 $45.45$   
 $35.45$

170

$\frac{1.43}{2.20}$

160

9.946538

$\frac{9.917891}{.43}$   
 $9.917891$   
 $1.407022$   
 $11.524913$   
 $9.946538$   
 $1.578375$

150

39.88

+ 02

1.36183'

140

1.657629'

4.53

+ 76

10.275470

11.825249

1.457629

Stone.

139

$\frac{10.167450}{94.55} = 55.47 \frac{1}{2}$

$\frac{4.53}{105.0} = .0427$   
 $\frac{90.5}{105.0}$   
 $105.0$

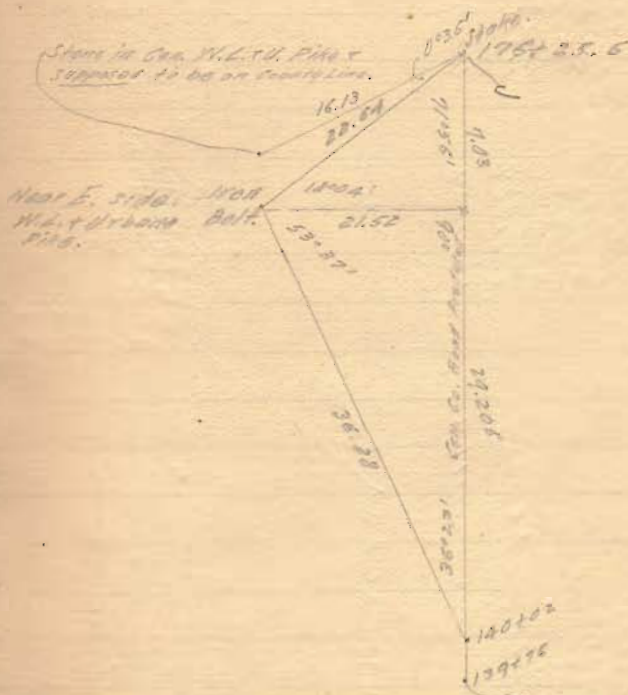
S.E. Cor. Sec. 21

State

1/4 Cor. Established as shown & cleared by clearing through online between S.E. & S.W. corners Sec. 21.

1/4 Cor. S side Sec. 21.

W.L. & Urbana Pike. (near W. side)



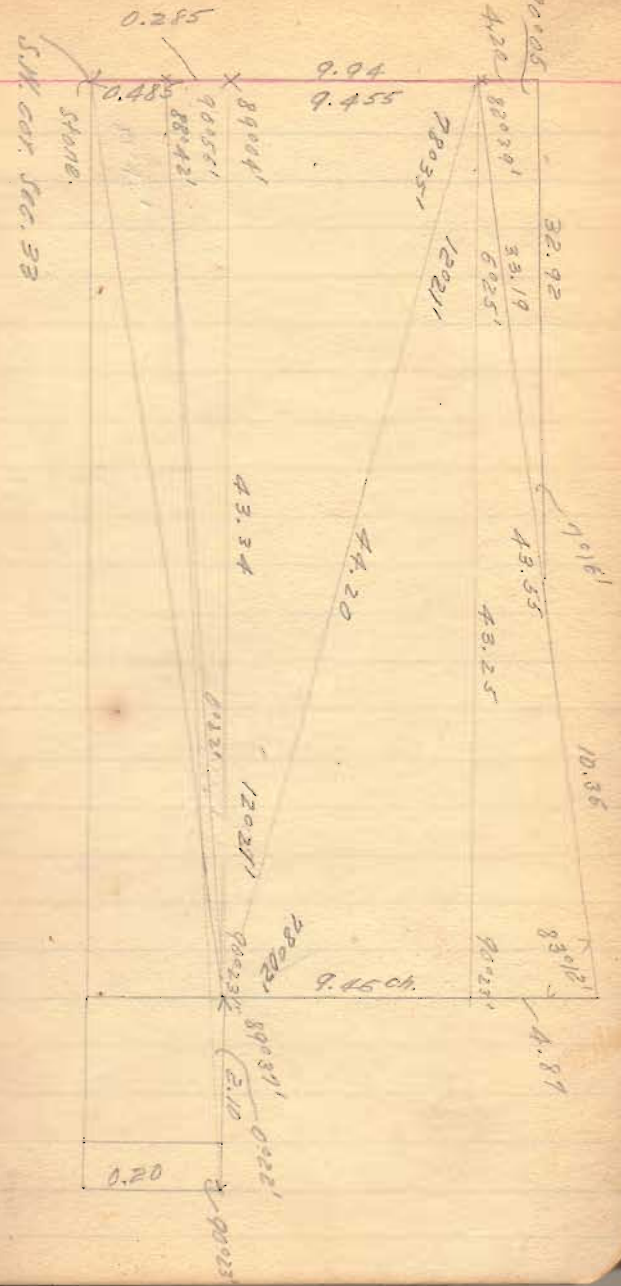
W side Sec. 21 S. 27.91 ch. to stone S.W. > Wagon's land. Set stake 15.41 ch. S. of stone.







S.W. Cor. Sec. 33 - 5-13



43.34  
 2.10  
 .21  
 45.55  
 42.985  
 2.665

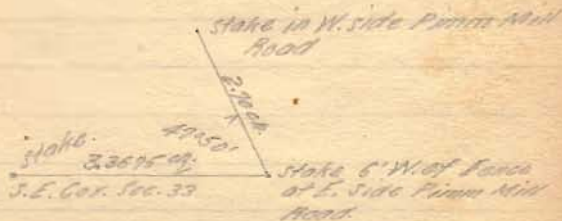
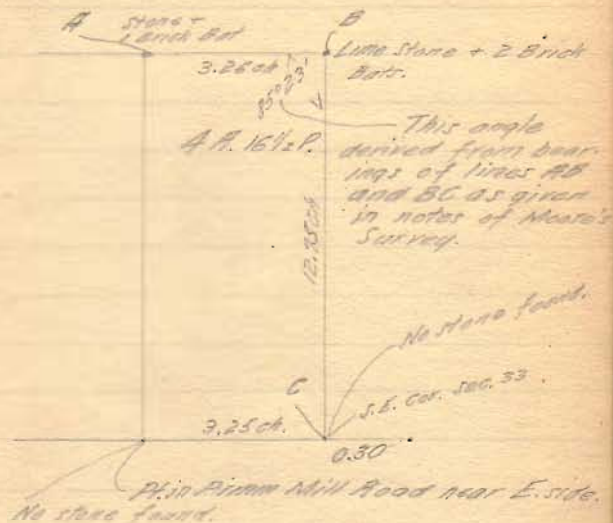
43.34  
 31.08  
 11.55  
 2785.97  
 42.985

43.34  
 42.985  
 0.355  
 1/4 Cor. S. side  
 Sec. 33.

S.E. Cor. Sec. 33-5-13

Notes of Surrey by H.C. Moore in 1859.

Found Corners A & B and established S.E. Cor. Sec. 33 from same in manner shown below.



Located S.E. Cor. Sec. 33 from  
Moore's Surrey.

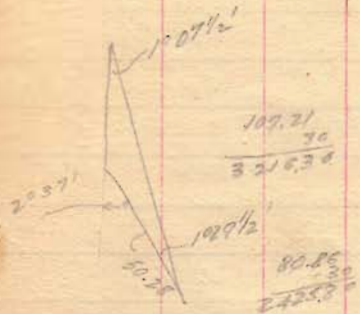


209.81  
 1049.65  
 209.81  
 3149.25

2 1/2 - 08 1/2  
 T. of 0-34 1/4 = 7.995198  
 + 3149  
 = 7999345

98.04  
 23.21  
 72.25  
 74.53

2.083543  
 179  
 2.083672 = 1.874076  
 2.995345  
 9.972421  
 2.083672  
 7.988739 = 2.0842



109.21  
 30  
 3226.38

8.289773  
 3126  
 8.292899

8.413008  
 2426  
 8.413494 = 50.28  
 1.701396

16.116889  
 2.292899  
 18.25990 = 56.68 AB = 49.78 0  
 66.68  
 18.90

8.204070 : 8.296207  
 1.991396 = 98.04

10.287603  
 8.204070  
 2.083533 = 1212.1  
 0.70  
 30



179.481  
 1-20 1/2  
 181-08 1/2

AB = 30.225  
 17.555  
 47.780  
 BC = 50.23  
 98.06  
 2.50

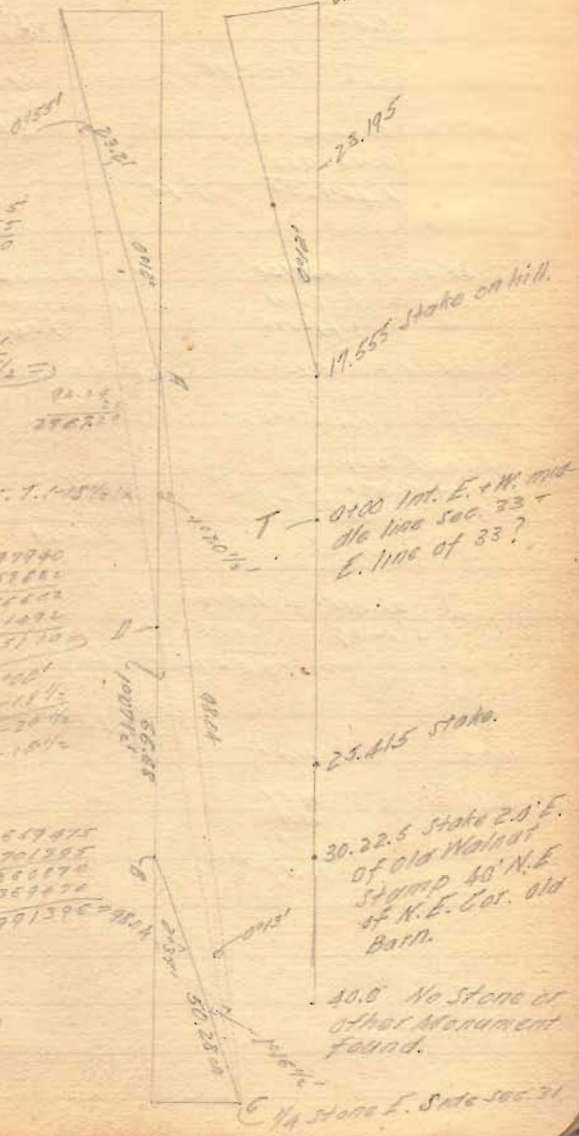
2 1/2 - 34 1/2  
 T. of 1-18 1/2 = 9.355195  
 2700  
 9.355662  
 98.06 : 2.00 :: T. of 1-08 1/2 = 9.14

1.991492 : 0.397940  
 2.252682  
 8.715662  
 1.991492  
 6.965170

19.2  
 289.70  
 1-18 1/2  
 1-20 1/2  
 1-18 1/2

8.266474  
 2899  
 8.260474 : 1.667475  
 1.701395  
 10.360890  
 1.269474  
 1.991596 = 98.04

23.30  
 17.555  
 30.225  
 50.23  
 121.260



1/4 stake E. Side sec 31

$$\begin{array}{r}
 10.135 = 1.005609 \\
 \quad 2.15 \\
 \hline
 1.005824 \\
 7.15309.442989 \\
 \hline
 10.40877 = 2.81
 \end{array}$$

$$\begin{array}{r}
 8.17 = 0.912222 \\
 7.15-70 = 9.442988 \\
 \hline
 1.469234 = 29.46
 \end{array}$$

$$\begin{array}{r}
 26.86 = 1.429106 \\
 5.74-70 = 9.983911 \\
 \hline
 1.446195
 \end{array}$$

$$\begin{array}{r}
 29.46 = 1.469233 \\
 9.983911 \\
 \hline
 1.485322
 \end{array}$$

$$\begin{array}{r}
 2.60 = 0.414973 \\
 5.17-09-9.469537 \\
 \hline
 9.384610 = 7668
 \end{array}$$

$$\begin{array}{r}
 30.075 = 1.580583 \\
 5.1-79 = 8.459301 \\
 \hline
 10.039884 = 1.099 \\
 \quad 769 \\
 \hline
 1.868
 \end{array}$$

78.93

$\begin{array}{r}
 81.02 \\
 1.75 \\
 \hline
 79.27 \\
 78.91 \\
 \hline
 78.93 \\
 78 \\
 \hline
 80.89
 \end{array}$

$$\begin{array}{r}
 10.98 \\
 2.31 \\
 \hline
 8.17
 \end{array}$$

$$\begin{array}{r}
 29.46 \\
 26.86 \\
 \hline
 2.60
 \end{array}$$

$$\begin{array}{r}
 91 \\
 17.09 \\
 \hline
 72.41
 \end{array}$$

$$\begin{array}{r}
 10.135 = 1.005609 \\
 5.74-70 = 9.983911 \\
 \hline
 1.021698
 \end{array}$$

$$\begin{array}{r}
 2.60 = 0.414973 \\
 5.72-51 = 9.910247 \\
 \hline
 0.395274 = 2.485
 \end{array}$$

$$\begin{array}{r}
 17.09 \\
 15.30 \\
 \hline
 1.39
 \end{array}$$

$$\begin{array}{r}
 29.075 \\
 2.485 \\
 \hline
 40.560
 \end{array}$$

$$\begin{array}{r}
 42.80 \\
 1.95 \\
 \hline
 40.38
 \end{array}$$

$$\begin{array}{r}
 30.57 \\
 2.485 \\
 \hline
 28.185
 \end{array}$$

$$\begin{array}{r}
 70.60 \\
 42.08 \\
 \hline
 38.52
 \end{array}$$

$$\begin{array}{r}
 70.59 \\
 42.05 \\
 \hline
 58.51 \\
 40.66 \\
 \hline
 1.95
 \end{array}$$



$$\begin{array}{r}
 3.475 \\
 10.52 \\
 \hline
 28.615 \\
 42.080 \\
 \hline
 92.68 \\
 40.560
 \end{array}$$

$$\begin{array}{r}
 82.64 \\
 1.96 \\
 \hline
 80.88
 \end{array}$$

71.91

State N.W. Cor. 33 0.33

E. of line.

80

70

61.85

60

51.12

50

40.885

30

20

17.04

16.74

10

0

N. 41° E

State S.W. Cor. Sec. 33

70.30 ch. E. of line

Line Hartzler Kirkwood

Line Kirkwood Int. + Wm. Kirkwood

1/2 State cor. 33 E. line Center of E. & W. Road.

Center  
Pike  
S. Side  
Pike

66.6	40.885
107.4	41.005
<u>41174.0</u>	<u>81.890</u>
13.5	.02
<u>40.50</u>	<u>81.91</u>
84.02	

81.15 1/2

81.13

80

81.13  
40.55  
40.58

70

60

50

48.83  
40.55

T.D. Line, D.R. 0.44'

40

30

20

10

0

N 86° W

0.16

40.55

Spike in Road

Stone 0.16 N. of Line. (Cor. 4-10-9-3)

$$\begin{aligned} 0.16 &= -1.304120 \\ 40.58 &= 1.607912 \\ \hline 7.595808 &= 0.16' \end{aligned}$$

B.M. in Road.

Stone  
Center Road

$$\begin{aligned} 40.55 & \overline{) 350.00.00} \\ & 72.10 \\ & \hline & 256.00 \\ & 24.30 \\ & \hline & 24.30 \end{aligned}$$

$$\begin{aligned} & 17.75 \\ & .0085 \\ & \hline & 106.50 \\ & 142.00 \\ & \hline & 152.55 \end{aligned}$$

Station  
S. E. Cor. Sec. 4

48.83  
40.55  
8.28

81.13  
40.55  
40.58) 16000 (394  
12194  
38200  
36502  
17880

.00784  
121  
8182  
722

2152  
0.35' N. of line. Cor. of 48.83

0.35' N. of line. Cor. of line and run West.



$$0.2375 = 4.375664$$

$$38.67 = 1.587274$$

$$75.8290 = 0.21'$$

80					
77.295	$\begin{array}{r} 15.45 \\ 38.625 \\ \hline 36.925 \end{array}$	$\begin{array}{r} 17.50 \\ 2.05 \\ \hline 75.45 \\ 1.84 \\ \hline 77.295 \\ 38.625 \\ \hline 38.670 \end{array}$	Stake 0.2375 S.W. Cor.	N. of Line.	Corrected line and ran W. with D.R. 1904
70					
60	$\begin{array}{r} 36.825 \\ .00616 \\ \hline 127300 \\ 36825 \\ \hline 220750 \\ \hline 22610550 \end{array}$	$\begin{array}{r} 2395 \\ 2 \\ \hline 714750 \\ 3 \\ \hline 714753 \\ \hline 20.3 \end{array}$	$\begin{array}{r} 0.23750 \cdot 00616 \\ \hline 23202 \\ 5480 \\ 3867 \\ \hline 76130 \end{array}$		
50					
40					
38.62 1/2	Corrected line ran W.		Stake 0.03 N.	of Line.	D.A. 0'21"
30					
29.10					Nail. Opp. old Stamp as Left.
20					
19.35					Stake
10					
0					Stake S.E. Cor. Sec. 10

83.15  
83.08  
83.00  
80

.305 S. of Cor.  
Corrected line from W.

Nail on Bridge  
S.E. Cor. 22 +  
S.W. Cor. 16  
Nail on  
Bridge  
State N. of  
E. end of Bridge

74.0325

Nail.

70

64.085  
62.38  
60

83.00  
8.9675  
74.0325

Nail.  
Land line Cor.

50

41.56 0.2058  
40  
30

.045  
09  
3  
7129  
4

41.56 / .04500 .00108  
41.56  
34.400  
18.06  
00108  
14.448  
18.06  
0195048

State.

20.77

Stone Nail  
Land line

20

18.06

Nail.

10

0 D.R. 1904 - 0°4' = 1900'  
Stone  
S.W. Cor  
Sec. 10  
+ S.E. Cor. 16

12.94 N. to N.E. Cor.  
Nail.  
12.22 S. to Cor.  
40.11 S. to 1/4 Cor.

Nail  
64.085 E. of E. end of Bridge.



9.825530: 9.858877  
0.919340 = 8.905  
10.778217  
9.825530  
1.352687 = 22.525  
41.56  
62.085  
62.38  
41.56  
20.77  
82.38 64.085  
1.705  
63.380

S. to 1/4 Cor. 80.50 Corrected line from W.

74.0325  
41.56  
32.47

83.15  
41.56  
41.59

41.59 / 30.500 .00133

32.47  
10733  
9741  
2962  
22729  
238025

29113  
13870  
12477  
13930

1 Cor. for 32.47

.205  
2  
610  
3

.305 = 7.484300  
41.59 = 1.688929  
.865211 = 0°25'

711830  
28

64.085  
41.56  
22.828  
22.933  
27.575  
27.575  
159.275  
16.51072

82.10

$\frac{12\frac{1}{2}}{3}$   
 $\frac{7136\frac{3}{4}}{5}$

80

76.44

70

65.22

$2 \overline{) 82.10}$   
 $\underline{41.05}$   
 $\frac{40}{1.05}$

60

58.84

50

$\frac{1225}{41.05} \quad 2 \overline{) 1225}$   
 $\underline{8125} \quad \frac{10612}{1225}$

41.05

40

$82.10 \quad 4900$   
 $\frac{15028525}{4925} \quad \frac{6612}{1025}$   
 $\frac{821}{252}$

30

22.93

20.27

20

10

0

$D.P. 0.001 - 0.005'$   
 $(0.005)$

Stake.

Nail in  
Carriage Plate.

Nail  
Stone 0.05

Nail.

Stake 1/4 Cor.

Stake.

Nail

Nail

S.E. Cor.  
100.22 +  
15.14 Cor. 16

0.12 1/4 S. of line.

$9.975080 \quad 9.975480$   
 $\underline{0.137140}$   
 $10.112620$   
 $\underline{9.975080}$   
 $0.840540$   
 $6.929$

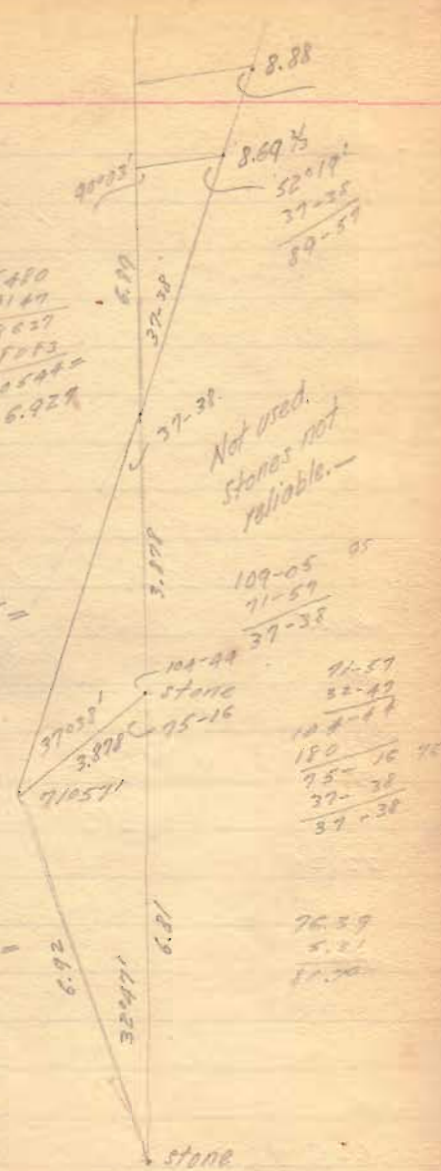
S. of line.

$9.975761 \quad 9.975480$   
 $\underline{0.582653}$   
 $10.574113$   
 $\underline{9.975761}$   
 $0.998352$   
 $6.143$

$9.975652 \quad 9.975769$   
 $\underline{0.732142}$   
 $10.566716$   
 $\underline{9.975652}$   
 $0.591064$   
 $3.878$

$1.939519$   
 $9.215761$   
 $\underline{0.725290} = 5.31$

$9.979519$   
 $9.548494$   
 $\underline{0.938013} = 6.89$   
 $3.88$   
 $10.77$



40.19

Stake

0.72 N. of line.

40

$$\begin{array}{r}
 0.72 = -0.857332 \\
 40.19 = \frac{1.604118}{.253212}
 \end{array}$$

30

20.095

Center Road

20

10

0

Run E. D.L. 1902'

1/4 Stone  
S. line 28

40.195

Stake S.W. cor  
166.28  
Nail

40

0.05 N. of line. 40.46 1/2 N. to 1/4 Stone  
S.E. Cor. Spelman's Hldg.  
N.E. Cor. Spelman's Hldg.

30

$$\begin{array}{r}
 40: 22.2 \\
 .85 \\
 40 \overline{) 11.10} \quad (2.77 = 2.84 \text{ Cor. for } 22.2) \\
 \underline{80} \\
 210 \\
 \underline{280} \\
 300
 \end{array}$$

22.20

Nail

20

10

4.25

Center Road  
To S.W. 1/4

0

Run W.

1/4 Stone  
S. line 28



80.71 2/3

80

80.72  
40.25  
40.47

66.01  
40  
26.01  
0.87122604  
2984.44  
71262 24 216  
37 48284  
21432

80.72  
136

66.01

66.01  
40.25  
25.76

50000.00  
0.516 S. of line.

25.06  
43.3  
7728  
7728  
103.04  
11154.07  
8094  
30000  
25.72  
12919

60

80.72 66.01

.893  
19863  
46209

50

52808  
57.62673 (713  
56.504

40.25 80.72

80.72

713 29 D.R. 0.137  
80.72  
31.558

40

.573

40 (A326  
34920  
35288

30

26.65

80.72  
26920  
24216

Long line  
D.R. 0.137

20

.22  
2  
44  
3

1 10.25  
21040  
16144  
48950

10

7133  
16

3850  
3850  
42900  
21000

0

D.R. 0.16

S.W. Cor  
Sec. 28

Stave. 0.871 N. of line.

50.06

5.503

90  
5.23  
84.38

91-33  
66-28  
158-07  
21-59

8.972289  
0.940500  
9.712789 = 0.5163  
1.

.713  
1.047  
636

18.25  
12.789  
5.503

9.572323 9.952288  
0.894412 = 7.843  
70.856970  
9.572323  
1.284747 = 19.25

273  
35  
634

7.843

10.07  
10.6531  
10079  
31033

0.740600  
9.998680  
0.738680 = 5.477

30.81  
5.48  
25.33  
19.25  
44.58  
40  
4.58

9.972289 9.126126  
1.106901 = 12.785

19.25

12.232835  
8.972289 = 12.26  
1.261559  
21  
35

9.972289 9.354271  
1.106901

10.260972  
9.972289 = 30.81  
1.488683  
19.25  
50.06



173  
44  
229  
212  
321

21.58

19.25

19.25

25.271

91°33'

7.843

13-04  
5-23 54  
9-41

80  
70  
60  
50  
40  
30  
20  
10  
0

Not used. Error  
in Angle.

Stone 14  
Col. Sec. 34

$$2.205 = 0.348409$$

$$5.2902' = 9.516027$$

$$1.07 = 0.020236$$

$$2.403$$

$$1.07$$

$$1.453$$

$$2.205 = 0.348409$$

$$5.2902' = 9.516027$$

$$1.07 = 0.020236$$

$$0.3752 = 9.771045$$

$$1.746 = 0.241391$$

$$5.52102' = 9.197320$$

$$1.376 = 0.138717$$

101-26

3.470

4.463

$$52-08$$

$$26-26$$

$$78-34$$

$$1.516$$

$$1.925$$

$$3.441$$

$$13.36$$

$$4.075$$

$$20.739$$

Not used  
Mistake  
in Angle.

$$5.653 = 0.752299$$

$$5.37-52 = 9.771045$$

$$3.470 = 0.540324$$

$$0.952299$$

$$9.907320$$

$$4.463 = 0.369590$$

$$20.739$$

$$3.443$$

$$25.202$$

$$14.51$$

$$39.712$$

$$14.105 = 1.170262$$

$$5.75-34 = 1.376189$$

$$14.31 = 1.161704$$

$$1.100409$$

$$5.11-55 = 9.297166$$

$$2.935 = 0.367573$$

$$2.935$$

$$3.471$$

$$6.403$$

$$7.439$$

$$1.074$$

(34+02')

0 0.12 1/4 N. of Stone.

80.187  
80

70

63.693

60

54.924

50

40.15

D.L. 0°17'

40

30

21.692

20

13.345

10

0

D.L. 1°04'

Stake  
S.W. Cor. Sec. 4  
1.052 N. of Stake

Stake  
S.W. Cor.  
Sec. 4

Stake. Sta. Cor.  
N. to Cor. Road

Stake  
405  
72.3

Stake

Cor. for 15.345

S.W. Cor.  
Sec. 24

2.205 = 0.343409  
5.34 = 2.942936  
1.234 = 0.091345

4.075 = 0.810125  
5.3500 = 9.991341  
= 0.679472

55-58  
29-02  
75-00  
37-52  
122-52  
170  
57-09

9.403  
2.924  
4.475

26-26  
57-08  
53-34

Road 40.04 (S.W. Road)  
to E. 36.195

2.528  
1.75  
1.177

80  
542  
351

2.205 = 0.343409  
5.3558 = 9.912404  
4.079 = 0.261873

4.075 = 0.610129  
5.5700 = 8.940294  
0.355 = -1.550824

1.234  
1.689 = 0.201124  
5.32-52 = 9.774509  
2.928 = 0.456574  
3.5408 = 9.924246  
2.46 = 0.370821

25-52  
57-08  
96-26  
150-00

4.475 = 0.550992  
30-22 = 9.924589  
2.428 = 0.385342

4.475 = 0.550993  
57-02 = 9.924246  
3.759 = 0.575089

14.545 = 1.170409  
6-26 = 9.044400  
1.659 = 0.219100  
2.328  
4.079

14.545 = 1.170409  
15-34 = 9.991259  
14.71 = 1.157655

12.745  
1.827  
4.02  
19.222  
2.860  
21.692  
3.759  
14.71  
40.151



89-35  
 19-19  
 7113  
 117  
 54.92  
 40.15  
 14.77  
 63.69  
 40.15  
 23.54

80.89 = 63.6991 = 1.0321 X

907941  
 39  
 907979

~~0.013700  
 1.99091  
 1.979781  
 1.990909  
 -1.990912 = .0127 Cor. for 63.693~~

60  
 54  
 221

4.087  
 7007  
 1225  
 4.9102  
 4.529  
 2832

~~0.013700  
 1.99091  
 1.979781  
 1.990909  
 -1.990912 = 7007 Cor. for 54.924~~

4.087  
 54  
 4.529

0.013700  
 1.603689  
 1.617385  
 1.907879  
 -1.909509

1.032  
 123  
 .909

909 = -1.958564  
 1.804091  
 1.762655  
 1.907179  
 -1.958776 = 7158  
 123  
 .931 Cor. for 63.693

Based on st. 118  
 between  
 corners.

~~-1.058564  
 1.729737  
 1.692295  
 1.907879  
 -1.990912 = 5192  
 123  
 .9402 Cor. for 54.924~~

22.54  
 19 1/2  
 271.86  
 2354  
 1147  
 40.74  
 4.59  
 40.59  
 5153  
 40.74  
 100904.087  
 5.036  
 1112  
 537  
 949  
 5.036  
 Cor. for 63.69



4.087 = 0.611405  
 16-52 = 9.462616  
 1408 = 7.148789  
 1408 = 1.148789  
 73-87 = 9.980904  
 13.79 = 1.129693  
 3.559 = 0.551084  
 16-52 = 9.462616  
 1.032 = 0.013700  
 3.559 = 0.551084  
 73-08 = 9.980904  
 3.404 = 0.531988

63.693  
 19.49  
 47.483  
 80.899  
 40.15  
 40.729  
 2.839  
 2  
 0.124 N  
 37.023  
 4095  
 off-line line  
 23.543  
 1.81  
 1.81  
 64.92  
 28.518  
 28300  
 14.77  
 19 1/2  
 13293  
 1477  
 738  
 2834  
 28301  
 10206  
 28300  
 28300  
 0.006  
 837  
 9076  
 Cor. for 54.92  
 4.087  
 499.66  
 4.629  
 3876



14.77  
 19 1/2  
 13293  
 1477  
 738  
 2834  
 28301  
 10206  
 28300  
 28300  
 0.006  
 837  
 9076  
 Cor. for 54.92  
 4.087  
 499.66  
 4.629  
 3876



80.097

80

70

60

56.82

50

40

39.92

30

20

18.425

10

0

Stone S.W.  
Cor. Sec. 10

86.10  
39.92  
44.18

39.92  
15.415  
27.495  
37  
150455  
64475  
1.03315  
29.92  
4915

201  
113  
Line Line.

1/4 Cor.

Nail in  
Edge of Ditch.  
1/4 Cor. Sec. 10  
N. of line

0.381  
0.308  
Corner stake

Stake.

Stone  
S.W. Cor. Sec. 4

79  
77-23  
78-37

3.045 = 0.483587  
11-22 = 9.295286  
2.801 = 1.778893

78-37  
19-19  
97-54  
180  
32-26

4.091 = 0.612572  
7-54 = 9.128128  
0.5633 = 1.950908

.501  
.507  
.027

39.96 1/2 N. 1/2  
40.53 S. 1/2

0.50 S. of Stone.

0.0377 N. of Stone.

3.045 = 0.483587  
78-37 = 9.991372  
2.916 = 0.474954

39.9  
0.38  
341

4.091 = 0.612572  
82-06 = 9.998359  
4.059 = 0.609437

24.58  
19.440

17.275  
12.54  
21.14  
112.90

56.11  
39.92  
15.90  
1.265  
15.635  
40.18  
24.555

354  
078  
72

39.92  
33.132  
4.059  
2.986  
80.097  
39.92  
40.177

.50  
49.38  
0.062 N.

80.10  
39.92  
40.18

37.29  
4  
23.9  
24.555  
49.174  
14.7350

40.18  
15.22  
12.54  
27.91

27.91  
27.91  
15.540  
56.101  
30.000

0.50

Stone



Arthur Holte  
Sept. 20. 1882

81.49

Stake 40'  
N. of line.

80

70

68.605

Land  
Line

Post  
Pole

61.26

Stake.

60

50

40.84

Stake.

Set 1/4 Stake at 40.745

40

30.84

Stake.

30

20.415

Nail at  
Stamp.

20

10

0

Stake  
S.W. Cor.  
Dec. 16

80.40

Flora,  
S. M. Cor.  
Sec. 22

80

70

60

50

40.22 D. I. 09121

W. Stone

40

39.78

Cor. D.S.  
14

30

20

10

0

S. M. Cor.  
Sec. 22

70.75

Stake

80

70

60

50

48.943

Nail

40.817

D. P. 0°56'

Stake

40

32.817

Nail

30

20

10

0

Stake  
S.W. Cor.  
Sec. 22

$$T = 0.25' = 2.007809$$

$$1.602494 + 1.376396$$

$$2.97889$$

25

$$9.384203$$

28

$$1.602494$$

12

$$7.781709 = 0.021'$$

56

31.917

3.126

40.043

27.991

$$8.126 = 0.909177$$

$$0.056' = 7.211895$$

$$(-1) 9.121772$$

$$.1329$$

50.86

48.943

31.917

48.943

31.917

0°56'

48.943

40.817

3.126

90.795

Stone

80

72.655

Loam  
Lime.

70

60

50

45.355

D.L. 0°04'

Stone.

40

30

20

10

0

D.L. 0°41'

S. E. Col.  
Sec. 34

80.415

Stone

80

70

60

50

40.27

D. B. 0°02'

1/4 Stone

40

30

20

10

0

N. 3°15' E.

S. W. Cor.  
Sec. 33

80

70

60

50

41.59

40

30

20

10

0

1/4 stone

S.W. Cor.  
586.34

No monument found.

2.009451

127

2.009578 = 1.296942

10.251757

11.651700

2.009578

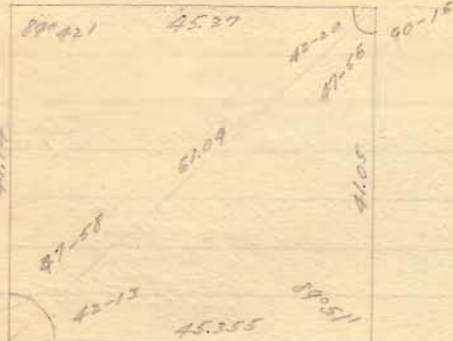
9.642122

66-01

23-41

89-42

42-30



45.355

2/90-09

41.05

45-00 1/2

86.205

1.936514

4.355

25

1.936539

0.623927

10.001137

10.635110

1.936539

8.697571

10.001011

725

70.001199

45-00 1/2

2-51 1/2

47-56

42-19

180-

47-57

2/32-02

66-01

9.527328 9.999999

1.613313

11.513312

9.727321

1.725984 = 41.09

41.12

102.27

19.05

9.528301 9.170846

6.812250 = 41.14

11.275110

9.227361

1.656109 = 45.27

42.4

3

127.2

42.1

25

126.2







9.9816361: 9.928911  
 0.974651 = 9.02  
 10.900982  
 9.9816361  
 1216 = 1.024002

89-49  
 44-27  
 45-20  
 150  
 120-40.  
 67-20

0.9790999  
 9.916361  
 0.527809 = 3.867

0.9790999  
 9.916361  
 0.549718 = 4.459

40.82  
 79.84  
 70.76  
 0.88

9.848206: 9.980999  
 1.601408  
 11.601409  
 9.848206

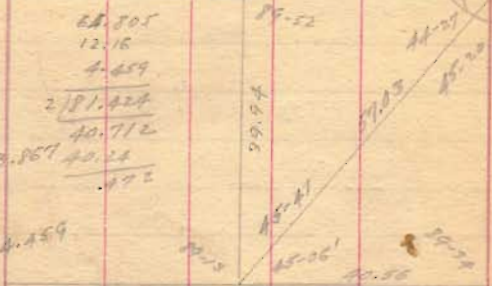
58.02 = 1.380131  
 40.40  
 99.42  
 10.62

41.05  
 12.16  
 4.959  
 51.424

9.999911: 9.851999  
 1.750121  
 11.601408  
 9.999911  
 1.501140 = 10.56

44.805  
 64.805  
 13.90  
 2.205  
 80.910

9.916361: 9.459088  
 0.974651  
 10.833788  
 9.916361  
 10.045  
 4.143  
 5.902 = 0.617218



1.907196: 1.944402  
 16.001411  
 9.948400  
 1.907196  
 9.028298

45-04  
 32  
 45-41  
 44-27

1.918623: 1.220192  
 10.579613 = 7.67-20  
 22-18  
 11.500108  
 1.318693  
 89-24  
 45-08  
 45-41  
 80-47

15.00  
 12.16  
 12.16  
 12.16

15.00  
 12.16  
 12.16  
 12.16

6.362  
 22.451  
 22.451

21-22-3-13

281  
 40.04  
 40.10

2090  
 40.24  
 40.50  
 41.16

14-53  
 14.022  
 40.07

40.13

Geo. A. Cox  
 40.12  
 40.12

40.12  
 40.12  
 40.12

S. L. Livingston  
 40.12  
 40.12

40.12  
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40.12  
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40.12  
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 40.12

40.12  
 40.12  
 40.12

21-22-3-13  
 40.85 PG. of  
 G. to left  
 120.89  
 40.11  
 281  
 40.54  
 51.23  
 40.85

40.30  
 40.30  
 40.30

40.30  
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40.30  
 40.30  
 40.30

40.30  
 40.30  
 40.30

© D. T. & L. Ry. 0.44 E. of 1/2 State.  
 Width of Mt. of Way 0.50 E. of ©  
 Hills on S. Line of Sec. 21  
 S. side 1/4 State Sec. 21 N. to Corn. Sec. 21

23.89  
16.61  
40.50  
7.28

2) 3-24  
1-42

2) 2-24  
1-12

2-24  
2-24

23.89  
0-59  
19-44

16.61  
2000  
1-25

1.607055

0.962131

11.492484

19.330533

1.287155

14.727130

8.563899  
1.607055

1.48 = 0.191454

1-42 90-42

0-12 87-56

2-00 1-25

1-24 89-21

90-02  
92-06

20.40

92005'

1.502121

9.327122

9.193253

1.507055

7.575798 = 0.013

92  
93  
59

1.606391  
7.861864  
9.468043

9.757109  
9.577350  
0.974051  
10.561437  
9.757109  
0.842567 = 6.262

9.757109  
9.926911  
0.974051  
10.900362  
9.757109  
13.90 = 1.143493

2.69 = 5.419752  
9.467860  
0.18767 = 1.54  
0.469452  
9.913215  
0.343490 = 2.205

64.8  
156  
2592  
3340

809  
809  
809  
1889  
1618  
2710  
2827  
2930

1.234 cor for 64.105

40.24  
1.56  
76096  
20120  
4024  
5663  
5379  
4858  
4950

767

90-13

59.10

45-00  
45-12 1/2

90-17  
45-05 1/2

45-13 1/2

150

184-46 1/2

4.21

12.52

44-45 1/2  
45-13

89-32

289-47

T. 44-53 1/2 =

44.405  
40.11  
70.885  
1.22

40.505

1.906229

29

1.906229

2.12

835

-1.352182

10.012519

9.755702

1.906229

7.454227 = 0.010

13.013393

125

10.013319

9.149327  
64

9.349391

9.900097

1.604010 = 40.18

11.504007

9.149391

1.756616 = 57.10

7.67-23

1.989543

67-03

40-03

77-83

16-09

22-10

19-05

45-12

42-44

19-59

10.300297

11.599503

1.979573

9.610619

12-10

112-24  
84-44

34-21

90-17

72-06

540

17-54

11-A2

1-24

90-06

17-56

2-00

89-56

90-06

90-17

14-01

89-56

90-06

90-17

14-01

360-00





27.44  
27.46

$27 = -2.928080$

$16.94 = 1.215502$   
 $7.517188 = 0.177$

90-37

19-23  
19-25  
90-100  
269-29

26

$16.57 = 1.219323$

$0.052 = 7.62002$

$4.185882 = 17$

12.14  
12.51  
15.25

19-29

16.54



18.46  
53  
57

19-39  
90-39  
19-29

270-13

$13 = -1.13943$

$11.72 = 1.092807$

$1.092807 = 0.055$

$2 =$

$1.092807 =$

$0.05 = -2.475127$

$17.95 = 1.455245$

$7.024572$

$0.05 = -2.671570$

$14.07 = 1.145134$

$7.550576 = 0.12$

90-49

19-09

269-29

19-59

90-37

530-27

720

152-15

$0.08 = -2.071151$

$25.74 = 1.410609$

$7.365522 = 11.1$

90-23

90-27

90-27

90-27

90-27

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90-27

90-27

90-27

90-27

90-27

90-27

90-27

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90-27

90-27

90-27

90-27

90-27

90-27

90-27

90-27

110

75-36

2791-26

45-12

43.44

37.44

92

$1.637890$

$1.573336$

$11.003032 = 7.45-12$

$11.576387$

$1.637890$

$9.938478$

40-59  
2-18  
86-09

$9.999019$

$9.999999$

$1.606811 = 40.44$

$7.606804$

$9.999019$

$1.606811 = 40.53$

$1.606811$

$9.999019$

$9.999999$

4-15

40-44

14-06

19-08

3.00

86-09

40.40

40.74

81.14

81.49

35

70

3

7210

30

90-16

89-44

180-00

89-59

269-59

77-43

77-43

77-43

77-43

77-43

77-43

77-43

77-43

32

3

785

114

89-17

30

89-27

76

76

76

76

76

76

76

76

76

76

89-17

14

89-31

90-23

16

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89-59

89-47

90-43

89-31

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41.50

40.95

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108

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46

90-01

40.60

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90-11

19-01

19-01

19-01

19-01

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19-01



40.96  
40.27  
51.23  
59

40.96  
3.49  
37.47

2/89.58  
44-50  
26  
1928

1.909716: -1.937849  
9.999748  
9.999797  
1.909716  
9.999797 - 0.028

90-25  
50-24  
95-51  
270-28  
26-20

9.152994: 10.  
1.612360  
11.612360  
9.152994  
1.750366 = 57.45

9.152745: 9.841540  
1.612145 = 408.4  
11.453789  
9.152745  
1.601043 = 39.91

2/89-40  
44-50

40.60  
39.92  
80.52  
68

1.905904: -1.822509  
9.999493  
9.829912  
1.905904  
9.924098

89-31  
44-21  
45-10

44-50  
0-29  
45-19  
44-21

9.851872: 9.999993  
1.608525 = 40.60  
11.608519  
9.851872  
1.756647 = 57.10  
39.51  
96.91  
12.29

180  
45-10  
134-20  
69-25  
23-13  
90-38  
44-12

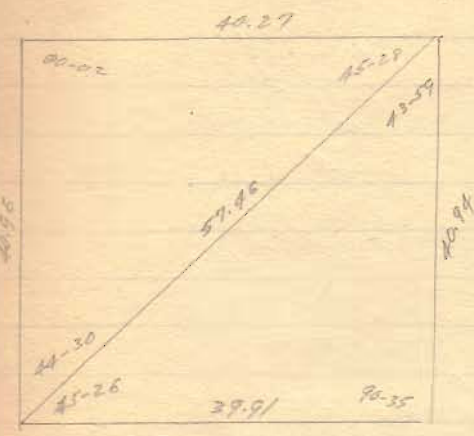
1.986309: 1.239795  
10.380992  
11.611787  
1.986309  
9.632418 = 23-13

38  
100  
16

6  
2  
242  
14

3/31/5  
90-24  
19-34  
40.44  
40.245  
15  
39.62  
19.5

40-24 84  
19-30  
45



89-27 87  
45-28  
23-59  
180  
136-01  
68-00 1/2

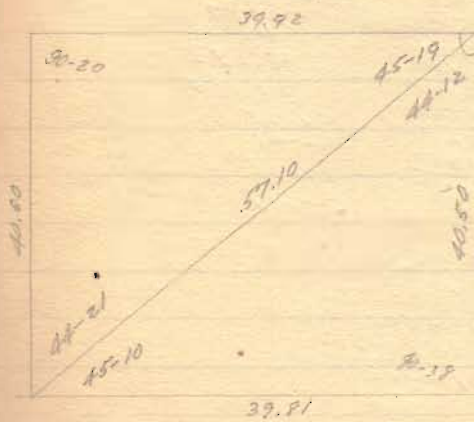
57.45  
46.94  
98.40  
15.52  
605  
20  
15 11/20

10.393590  
182  
10.393772

1.992995: 1.218010  
10.393772  
11.811792  
1.992995  
9.618787

61-00 1/2  
27-34 1/2  
90-35

45-26  
44-30  
89-56



89-31

20  
7/60  
0

90-29  
5  
60-20

9.999973: 9.858745  
1.756647  
11.609292  
9.999973  
9.632418 = 40.50

42.50  
12.50

89-29  
90-30  
90-31

9.361822; 9.925384

0.477121

90-30

90-40

19-51

10.402505

9.361822

1.040683 = 10.95

2.50  
1.95  
4.45

9.999982; 9.530915

1.040683

10.571598

9.999982

0.571616 = 2.229

4.45

0.72

.72

3.73

9.999982; 9.974792

1.040683

11.015475

9.999982

1.015493 = 10.36

40.74  
40.25  
81.19  
.59

45.02 1/2  
20.26

1.309296

2) 90-29

45-26 1/2

1.231849

10.00 11 3/4

9.889810

1.90 5320

7.952574

10.0010 1/4

12.5

10.0010 1/4

40.25

89-51

45-34

90-24

44-50

50-34

45-25

45-24

40.25

89-36

2) 135-10

67-55

9.853758;

9.909599

1.612148 = 40.94

7.672147

9.853758

1.784409 = 57.34

1.214579

1.22

7.214773

10.384505

11.599277

1.992479

9.606790

40.945

78.283

18.395

67-35

22-01

89-56

45-30

1.992489;

9.999989;

9.808218

1.753709

11.500607

9.999989

1.500607 = 41.43

Stamps

0.13

1337 5.205

1459 21.38

1596 37.19

1600 40.38

1782 64.93

1857 74.93

Stamps

0.19

80.70

40.38	40.38	40.38	40.38	40.38
38.175	19	3.19	24.55	24.55
5.205	21.38	37.19	64.93	74.93
.06				5.74
80.7	1037	21.38		50.84

24.21	13	21.38		37.19
6020	13	.06		.06
56.48	13	1.2828	1159	223.14
		80.7	13	15.14
		47.58		6.174
		40.35		56.49
		72.71		5.250

40.38		64.93		74.93
.06		.06		.06
24.21	(3)	2.8958	(14.82 30.7)	44.958
		22.27		40.35
5.77		6.678		4.608
.06		54.56		40.35
80.7		2.220		5.730

32.25	1858	79-19
134.0		90-41
30.7		30
55.24		71-11
		30
70-24		90-41
13		
90-41		

61.4		19
.06		.03
84		40.34
84		5700.614
209.24		40.34
12		10000
1848		
322		
11.081		

0.165 54010

152

.143 30.09

.135 26.99

.133 25.42

.120 19.43

10.09 16.67

0.152  
 < 2525 > 10.42

5555 10.42

0.152 .078  
 0.23

0.165  
 0.152  
 0.319  
 0.23  
 .089

10.42  
 .089  
 7294

833.5  
 40.16 ) 9055.4 (225 .0225  
 8032  
 10234  
 8032  
 2202

19.43  
 .089  
 13501  
 15444

40.16 ) 1.5192 (042  
 16064 .078  
 8301 .120

16.67  
 .089  
 11529  
 11388

25.42  
 .089  
 17794  
 20336

40.16 ) 2.21154 (055  
 20080 .078  
 20354 .133

16.67  
 .089  
 159  
 216

30.09  
 .089  
 21069  
 24072

40.16 ) 2.61223 (055  
 24096 .078  
 20923 .143

16.67  
 .089  
 199  
 216  
 20080 .078  
 20100 .132

.165  
 .152

.317  
 .23

.089  
 2

.177  
 2

7.522  
 7

89-35.1  
 89-45